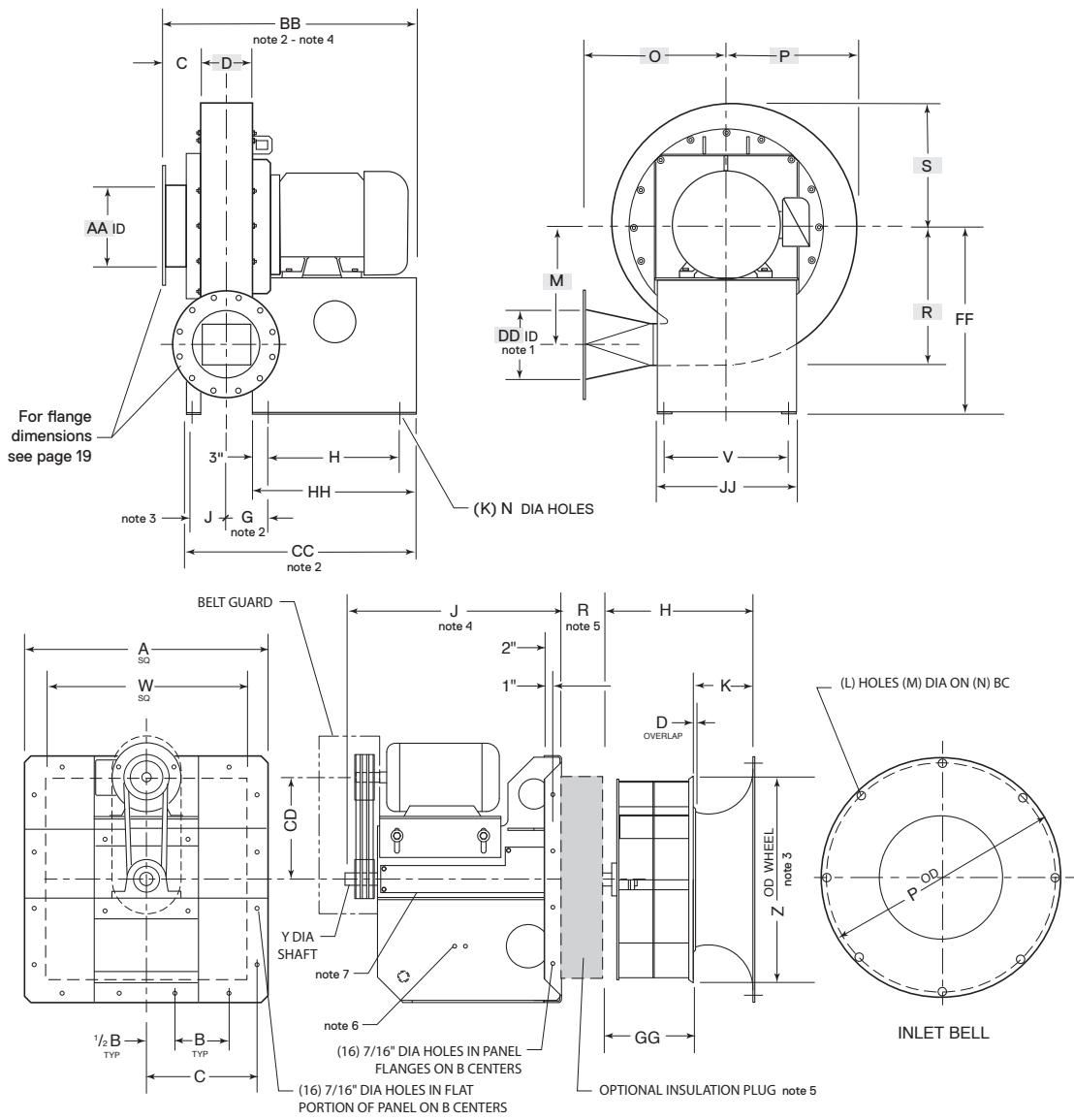


# Engineering Data

OEM AND INDUSTRIAL AIR HANDLING SPECIALISTS

CINCINNATI FAN



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## TERMS AND DEFINITIONS

**Ahp** – Air Horsepower, is work done by the fan expressed as horsepower.

$$Ahp = \frac{CFM \times TP}{6356}$$

**bhp** – Brake Horsepower, is the horsepower absorbed by the fan.

**BTU** – British Thermal Unit, is the amount of heat required to raise one pound of water from 63°F to 64°F.

**CFM** – Cubic Feet Per Minute, is the volume of air moved per minute.

**Capture Velocity** – The air velocity at any point in front of a hood or at the hood opening necessary to overcome opposing air currents and capture the contaminated air by causing it to flow into the hood.

**Conveying Velocity** – The minimum air velocity required to move or transport particles within a duct system. Measured in feet per minute.

**Drive Losses** – Power lost in overcoming friction from the belt, pulley and bearing friction.

**EDR** – Equivalent Direct Radiation, is the amount of heating surface which will give off 240 BTU per hour.

**fpm** – Feet Per Minute, is the velocity of the airstream.

**Final Temperature** – is the temperature of air after passing over heating coils under specified conditions

**Free Air Delivery** – is the condition under which a fan operates when no static pressure or resistance is present.

**hp** – Horsepower, is the actual rated output of the fan motor used.

**ME** – Mechanical Efficiency, is the ratio of horsepower absorbed (bhp) to horsepower delivered by the fan (Ahp).

$$ME = \frac{Ahp}{bhp}$$

**Plenum Chamber** – is an air compartment maintained under pressure to serve one or more distributing ducts.

**RPM** – Revolutions Per Minute, is the number of times the fan shaft revolves per minute.

**Replacement Air** – The term has been used in the same context as supply air, make-up, and in-take air. It introduces fresh outside air into a structure to replace air exhausted from fans.

**Standard Air** – is air which weighs .075 pounds per cubic foot, which is dry air at 70°F dry bulb with a barometric pressure of 29.92 inches of mercury.

**SE** – Static Efficiency, is expressed as:

$$SE = \frac{CFM \times SP}{6356 \times bhp}$$

**SP** – Static Pressure, is a measure of the force exerted by the fan in moving air through any ventilating system.

**Stall** – A region of instability on a fan performance curve. Evidence of this region is a dip in the performance curve, also a drop in the bhp curve. It is caused by the separation of the air flow from the surface of the propeller blade or fan wheel.

**Shut Off** – is the point of operation where the fan flow rate is zero.

**System** – The path through which air is pushed or pulled. This normally includes ducts, coils, filter, plenum changer, etc., through which air flows. A system can be as simple as inducing air motion into a space or a network of ducts providing air for multiple locations.

**TE** – or Total Efficiency, may be expressed as:

$$TE = \frac{CFM \times TP}{6356 \times bhp}$$

**TS** – Tip-Speed, is the peripheral speed in feet per minute of a propeller tip or fan wheel at any specified RPM.

**TP** – Total Pressure, is the sum of the static pressure (SP), and velocity pressure (VP) at any given point in a ventilating system.

**V** – Velocity, is equal to the flow rate (CFM) divided by the cross-sectional area of the air flow.  $V = CFM \div \text{Area (sq ft)}$

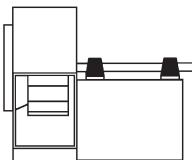
**VP** – Velocity Pressure, is equal to the kinetic energy per unit volume of the flowing air. It can be calculated from the formula.

$$VP = \left( \frac{fpm}{4005} \right)^2$$

**Transport Velocity** – See Conveying Velocity.

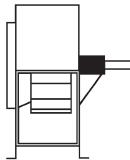
## FAN ARRANGEMENTS AS DEFINED BY AMCA

**SW** - Single Width



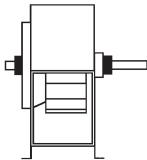
**Arrangement 1 SWSI** For belt drive connection. Impeller overhung. Two bearings on base.

**DW** - Double Width



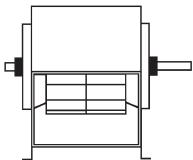
**Arrangement 2 SWSI** For belt drive or direct connection. Impeller overhung. Bearings in bracket supported by fan housing.

**SI** - Single Inlet

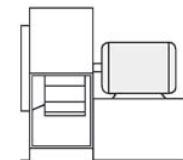


**Arrangement 3 SWSI** For belt drive or direct connection. One bearing on each side and supported by fan housing.

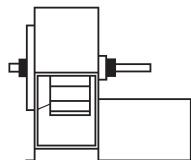
**DI** - Double Inlet



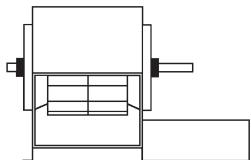
**Arrangement 3 DWI** For belt drive or direct connection. One bearing on each side and supported by fan housing.



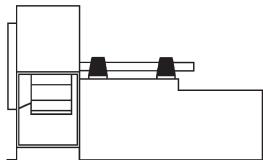
**Arrangement 4 SWSI** For direct drive. Impeller overhung on prime mover shaft. No bearings on fan. Prime mover base mounted or integrally connected.



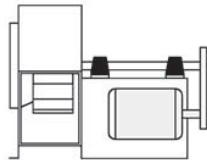
**Arrangement 7 SWSI** For belt drive or direct connection. Arrangement 3 plus base for prime mover.



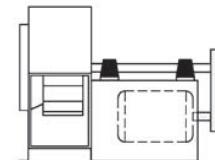
**Arrangement 7 DWI** For belt drive or direct connection. Arrangement 3 plus base for prime mover.



**Arrangement 8 SWSI** For belt drive or direct connection. Arrangement 1 plus extended base for prime mover.



**Arrangement 9 SWSI** For belt drive. Impeller overhung, two bearings, with prime mover outside base.

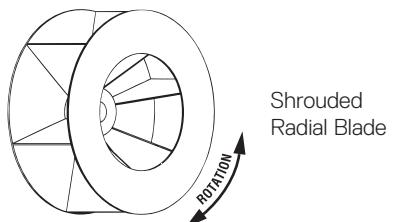


**Arrangement 10 SWSI** For belt drive. Impeller overhung two bearings, with prime mover inside base.

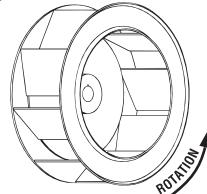
## ROTATION AND DISCHARGE DESIGNATIONS



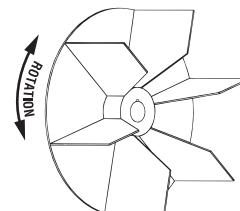
## WHEEL TYPES



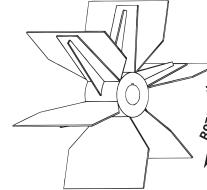
Shrouded Radial Blade



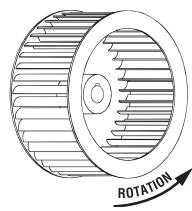
Backward Inclined



Open Radial Blade



Open Paddle Wheel  
(not available from Cincinnati Fan)



Forward Curve  
(squirrel cage)

- 1 Direction of Rotation is Determined from Drive Side of the Fan.
- 2 On single inlet fans, drive side is always considered as the side opposite fan inlet.
- 3 On double inlet fans with drives on both sides, drive side is that with the higher powered drive unit.
- 4 Direction of discharge is determined in accordance with diagrams. Angle of discharge is referred to the vertical axis of fan and designated in degrees from such standard reference axis. Angle of discharge may be any intermediate angle as required.
- 5 For fan inverted for ceiling suspension, or side wall mounting, direction of rotation and discharge is determined when fan is resting on floor.

## FAN LAWS AND FORMULAS

### Basic Fan Laws

Variable	When Speed Changes	When Density Changes
Volume (CFM <sub>1</sub> )	Varies Direct with Speed Ratio $CFM_2 = CFM_1 \left( \frac{RPM_2}{RPM_1} \right)$	Does Not Change
Pressure (P <sub>1</sub> )	Varies with Square with Speed Ratio $P_2 = P_1 \left( \frac{RPM_2}{RPM_1} \right)^2$	Varies Direct with Density Ratio $P_2 = P_1 \left( \frac{D_2}{D_1} \right)$
Horsepower (hp <sub>1</sub> )	Varies with Cube with Speed Ratio $hp_2 = hp_1 \left( \frac{RPM_2}{RPM_1} \right)^3$	Varies Direct with Density Ratio $hp_2 = hp_1 \left( \frac{D_2}{D_1} \right)$

### To Calculate:

$$\text{Velocity} = \text{CFM} \div \text{Duct Area (sq ft)}$$

Alternate Method:

$$\text{Velocity} = \frac{\text{CFM} \times 144}{\text{Duct Area (sq in)}}$$

$$\text{CFM} = \text{Velocity} \times \text{Duct Area (sq ft)}$$

Alternate Method:

$$\text{CFM} = \frac{\text{Velocity} \times \text{Duct Area (sq in)}}{144}$$

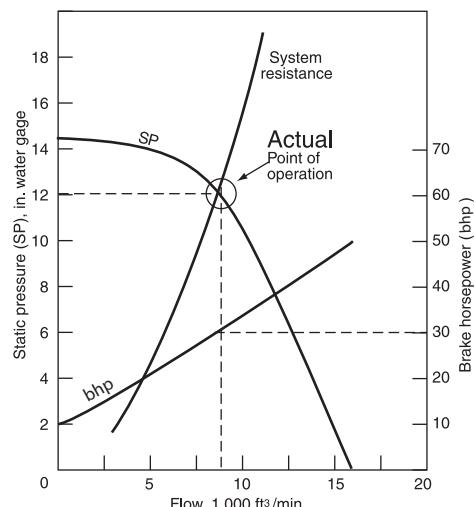
$$\text{Tip Speed} = \text{Circumference} \times \text{RPM}$$

$$bhp = \frac{\text{Total Watts input} \times \text{Motor efficiency}}{746}$$

$$\text{Mechanical Efficiency} = \frac{\text{TP} \times \text{CFM}}{6356 \times \text{bhp}} \times 100\%$$

$$\text{Static Efficiency} = \frac{\text{SP} \times \text{CFM}}{6356 \times \text{bhp}} \times 100\%$$

The fan's actual operating point is at the intersection of its static pressure curve and the system's resistance curve.



### Corrections for Density Rarefaction

When negative static pressure exists on the inlet side of a fan, additional correction for a lower density should be made when the negative pressure is 20"WG or more. When the negative pressure is less than 20" this factor is usually considered negligible unless the system designer is calculating to extremely close tolerances. The chart at right shows correction factors for negative inlet pressure. The factors apply to static pressure and brake horsepower in the same manner as temperature and altitude corrections.

Correction Factors for Rarefaction (negative inlet pressure)

Static Pressure	Factor
5	1.01
10	1.03
15	1.04
20	1.05
25	1.07
30	1.08
35	1.09
40	1.11
50	1.14
60	1.17

### Calculation of WR<sup>2</sup> (or WK<sup>2</sup>) of Fan Wheel

$$WR^2 = \left( \frac{\text{Wheel weight}}{\text{in pounds}} \right) \times \left( \frac{\text{Wheel radius in}}{\text{feet} \times GY} \right)^2$$

GY = .90 for Forward curved wheels.  
.70 for Backward inclined and shrouded radial wheels.  
.67 for Open radial wheels

WR<sup>2</sup> is expressed in: lb - ft<sup>2</sup>

### Guideline to Determine the Spread and Throw of a Mancooler

These calculations are for determining the velocity from a fan and also the width of the stream at a specific distance. While these values are influenced greatly by the presence or absence of walls, floors and obstruction, the following formulae will give a good approximation for most cases.

#### Spread:

$$W = .36L + \frac{d}{12}$$

W = Maximum width in feet of airstream perpendicular to axis of rotation of the fan.

L = Distance from fan in feet.

d = Fan diameter in inches

**Velocity:** (not less than 10 feet from fan)

$$(1) k = 5 \left( \frac{2.5 \times \text{CFM}}{d} \right)^2$$

$$(2) ^vLa = 115 - \sqrt{\frac{k}{L}}$$

$$(3) ^vmax = \left( \frac{d}{73} + 1 \right) ^vLa$$

k = Fab constant

$^vLa$  = Average velocity across the width of the spread. L feet from the fan (fpm).

$^vmax$  = Maximum velocity. L feet from the fan (fpm)

CFM = Free Air Delivery of fan.



## MATERIAL CONVEYING

Bulky materials such as those shown in **Table 1**, can be conveyed pneumatically using a Cincinnati Fan **RBE series** pressure blower. Follow the steps below to determine the PBS blower best suited for your application.

Example: Assume a requirement to move 2400 pounds per hour of barley through 200 feet of straight, horizontal, round duct.

Note: For each 90° elbow in your duct system, add 20 feet of straight duct to determine total equivalent straight duct length.

For each 10 feet of vertical duct, add 10 feet to your total straight duct length.

- I Convert pounds per hour to pounds per minute:  $2400 \text{ lb/hr} \div 60 = 40 \text{ lb/min}$
- II Refer to **Table 1**. Find barley under material (column A) and read horizontally. Barley weighs 38 pounds per cubic foot (column B), requires 38 CFM of air per pound of material (column C) and a minimum of 5000 feet per minute conveying velocity (column D).
- III Determine the minimum cubic feet per minute (CFM) requirements:  

$$\begin{array}{rcl} \text{CFM/lb of material} & & 38 \text{ (from column C)} \\ \times \quad \quad \quad \text{lb/min} & = & 40 \text{ (from step I)} \end{array}$$

1520 Total minimum CFM required @ 5000 ft/min conveying velocity (column D)
- IV Determine the system static pressure requirements from **Table 2**. Read across the 5000 ft/min velocity line to the 8" duct size column since this is the first (smallest) duct size column over 1520 CFM.  
 We have selected 8" duct size with 1745 CFM (actual) to maintain a velocity of 5000 ft/min.  
 The friction loss is 6.02" SP per 100'  $\times 2 = 12.04"$  plus 3.5" SP suction pickup (column E, **Table 1**) = 15.54" total system static pressure for 200 feet of straight 8" duct.
- V Check fan rating tables for 1745 CFM at 15.54" SP at the lowest horsepower. From the RBE Exhaust Blower engineering data catalog we suggest a Model RBE-9. Interpolate 3499 RPM, 7.59 bhp.
- VI If material being conveyed will be going through the fan, the fan bhp can be significantly increased. The approximate increase is calculated as:

$$\text{Actual bhp} = \frac{\text{lb/minute of air} + \text{lb/minute of material}}{\text{lb/minute of air}} \times \text{fan bhp (7.59, step V)}$$

In this example :  $\text{lb/minute of air} = 1745$  (actual CFM, step IV)  $\times .075 \text{ lb/ft}^3$   $\left( \frac{\text{Standard}}{\text{Density}} \right) = 130.9$

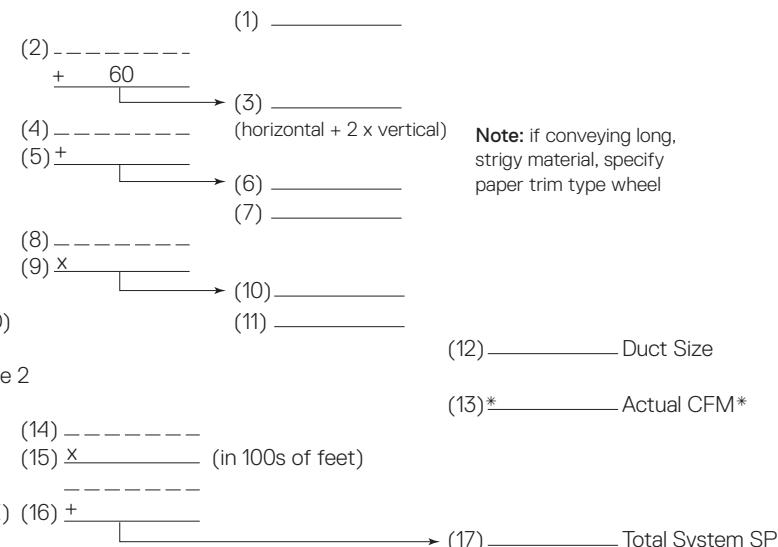
$$\text{Therefore: } \frac{130.9 + 40}{130.9} = \frac{170.9}{130.9} = 1.31 \times 7.59 + 9.94 \text{ actual bhp} \quad \text{note 3}$$

### Note

- 1 For each 10 feet of vertical duct, add 10 feet to your total straight duct length.
- 2 For equivalent losses through elbows, see chart on page 9 of our Engineering Data catalog.
- 3 Make sure you use correct density for location of fan.

## MATERIAL CONVEYING CALCULATION

- (1) Material Being Conveyed
- (2) Pounds Conveyed/Hour
- (3) Pounds/Minute
- (4) Feet of Straight Horizontal Duct
- (5) Number of 90° Elbows
- (6) Total Equivalent Feet of Duct
- (7) Material Weight, lb/ft<sup>3</sup> (col. B)
- (8) CFM/Pound of Material (col. C)
- (9) Pounds/Minute (step 3)
- (10) Total Min. CFM Required
- (11) Min. Conveying Velocity in FPM (col. D)
- (12) Duct Size to Get Total CFM (step 10)  
@ Minimum Velocity (step 11) per table 2
- (13) Actual CFM for Duct (step 12)
- (14) Friction Loss/100 ft
- (15) Total Equivalent Feet of Duct (step 6)
- (16) Suction Pickup in inches of WC (col. E)
- (17) Total System SP



Fan Model to get #13 (actual CFM) and #17 (total SP) above \_\_\_\_\_

Fan RPM \_\_\_\_\_

Actual Fan bhp \_\_\_\_\_ Step VI

\*Must be equal or greater than step 10



## AVERAGE AIR CHANGES REQUIRED FOR GOOD VENTILATION

Type	Minutes per Change	Type	Minutes per Change	Type	Minutes per Change
Assembly Halls	2-10	Engine rooms	1-3	Laboratories	1-5
Auditoriums	2-10	Factories	2-5	Laundries	1-3
Bakeries	2-3	Forge Shops	2-5	Offices	2-10
Boiler Rooms	1.5	Foundries	1-5	Packing Houses	2-5
Bowling Alleys	2-10	Garages	2-10	Plating Rooms	1-5
Churches	5-15	Generator Rooms	2-5	Toilets	2-5
Dairies	2-5	Gymnasiums	2-10	Transformer Rooms	1-5
Dance Halls	2-10	Kitchens - Hospital	2-5	Warehouses	2-10
Dry Cleaners	1-5	Kitchens - Restaurant	1-3		

Formula to determine fan capacity:

$$\text{CFM Required: } \frac{\text{Volume of space (W x L x H)}}{\text{Number of minutes per air change}}$$

Note—The above chart is a general guideline only.

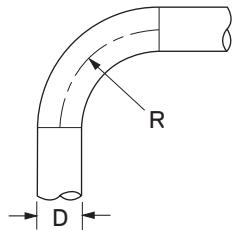
## RECOMMENDED VELOCITIES FOR EXHAUST HOODS

Area of Slot or Face (sq ft) x Velocity (fpm) = CFM Required

Process Type	Type of Hood	Required Air Velocity Average
Aluminum Furnaces	Enclosed hook, open on side Canopy hood	150-200 fpm over open face 200-250 fpm over face
Bottle Washing	Enclosed Booth	150-250 fpm over face
Brass Furnaces	Enclosed hook, open one side Canopy hood	200-250 fpm over open face 200-250 fpm over open face
Chemical Laboratories	Enclosed hook, door front Enclosed hook, open front Down draft, table type	100 fpm over door opening 100 to 150 fpm over face 150 to 200 fpm over table gross area
Degreasing	Canopy hood Slot type for tanks up to 4' wide (slot one side)	150 to 200 CFM over face 2' width use 1500 to 2000 fpm through 2" slot 3' width use 1500 to 2000 fpm through 4" slot 4' width use 1500 to 2000 fpm through 6" slot For tanks over 4' use slots on four sides
Driers	Canopy hood Slot type at each end continuous drier	125 to 150 fpm over face 150 to 200 fpm over 6" to 8" slot
Electric Welding	Enclosed booth, open front Canopy hood	100 to 150 fpm over face 125 to 150 fpm over face
Electroplating	Canopy hood Slot type for tanks up to 4' wide (slot one side)	1250 to 1750 fpm over face 2' width use 1500 to 2000 fpm through 2" slot 3' width use 1500 to 2000 fpm through 4" slot 4' width use 1500 to 2000 fpm through 6" slot For tanks over 4' use slots on four sides
Foundry Shake Out	Enclosed booth, open front Down draft grill type	150-200 fpm over face 300-500 fpm
Grain dust, wood, flour, etc	Slot types Canopy hood	2000 fpm through 2" to 4" slot 500 to 600 fpm over face
Grinding (disc) and sanding	Down draft, grill type Bench type with slot one side	400 fpm over open face 2000-2500 fpm through 4" slot
Hood forge	Canopy hood Enclosed booth, one side	150-200 fpm over face 200-300 fpm over face
Kitchen Ranges	Canopy hood	125-150 fpm over face
Metal Spraying	Enclosed hook open one side	200-250 fpm over face
Paint Spraying	Enclosed hook open one side	125-200 fpm over face
Paper Machine	Canopy type	100-300 fpm over face
Pickling Tanks	Canopy type Slot type for tanks up to 6' wide, slot one side only	200-250 fpm over face Minimum 4" slot 2000 to 2500 fpm through slot
Quenching Tanks	Canopy type	200-300 fpm over face
Rubber Mixing Rolls	Canopy type Slot type	150-200 fpm over face 2000 to 2400 fpm through 2" slot
Soldering Booths	Enclosed booth, open one side	150-200 fpm over face
Steam Tanks	Canopy type Slot type for tanks up to 6' wide, slot one side only	200 fpm over face 1500-2000 fpm through minimum 4" slot
Stone Cutting	Enclosed booth, open face	400-500 fpm over face
Varnish Kettles	Canopy type Slot type, all around slot	250-350 fpm over face 2" minimum slot 2000 fpm through slot

## DUCT DESIGN PRACTICES

Equivalent Resistance in Feet of Straight Pipe

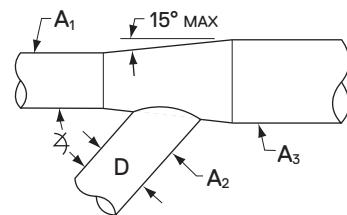


For 60° elbow -  $0.67 \times$  loss for 90°

For 45° elbow -  $0.50 \times$  loss for 90°

For 30° elbow -  $0.33 \times$  loss for 90°

Equivalent Entry Losses in Feet of Straight Pipe



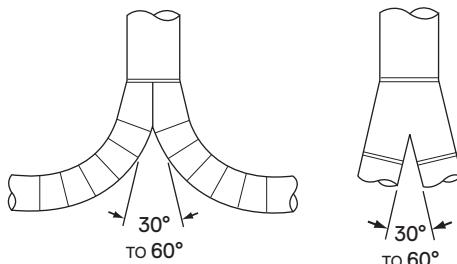
$$A_3 = A_2 + A_1 \quad A = \text{Area}$$

Diameter of Duct (D)	90° Elbow Centerline Turn Ratio (R)*		
	1.5	2.0	2.5
3"	5	3	3
4"	6	4	4
5"	9	6	5
6"	12	7	6
7"	13	9	7
8"	15	10	8
10"	20	14	11
12"	25	17	14
14"	30	21	17
16"	36	24	20
18"	41	28	23
20"	46	32	26
24"	57	40	32
30"	74	51	41
36"	93	64	52
40"	105	72	59
48"	130	89	73

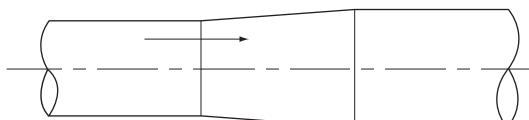
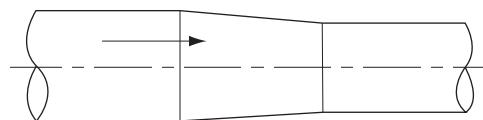
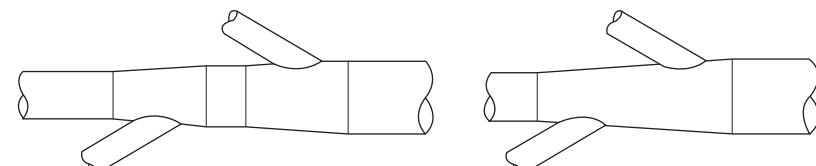
\* Turn Ratio = Number of duct diameters

Diameter of Duct (D)	30° $\angle$	45° $\angle$
4"	3	5
6"	5	7
8"	7	11
10"	9	14
12"	11	17
14"	13	21
16"	16	25
18"	18	28
20"	20	32
24"	24	37
28"	28	46
30"	31	49
32"	33	53

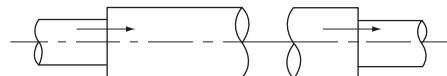
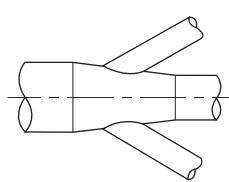
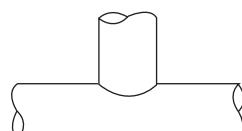
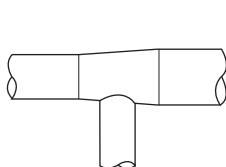
### Preferred



### Acceptable



### Avoid



## TYPICAL ENTRANCE LOSSES

Orifice Type	Description	Loss*	Orifice Type	Description	Loss*
	Smooth well rounded	5%		Unflanged cone 15° per side	13%
	Two-cone 45° and 15° per side	6%		Flanged pipe	50%
	Flanged cone 15° per side	7%		Unflanged pipe	90%

\* Loss in percent of velocity pressure (% VP)

## GOOD DUCT INSTALLATION GUIDELINES

Air performance ratings in fan catalogs were derived from tests and test procedures in accordance with the latest Air Moving and Control Association (AMCA) standards. The test procedure used for centrifugal fans, for example, includes a straight outlet duct and open inlet. Laboratory test conditions are seldom, if ever, found in actual field installations. A poor fan inlet or outlet condition will result in an increase in system pressure losses which will reduce the fan's performance and decrease motor efficiency. Increased noise levels may also be caused by certain duct designs.

### Open or Abrupt Discharge

When the exhaust air of a fan is discharged into an open area, large duct, or plenum chamber, the abrupt expansion of the air flow pattern and the sudden, reduced air velocity creates an air turbulence that increases the system static pressure which reduces fan performance. Up to 20% of the air volume can be lost due to a poor outlet condition. A duct extension with a minimum length of three times the fan wheel diameter should be added to the fan outlet.

### Discharge Duct Turns

Duct turns (elbows) located near the fan discharge should always be in the direction of the fan rotation to minimize duct turbulence.

Air flow is also reduced when the elbow is too close to the fan discharge. A minimum length of four times the wheel diameter of straight duct should be installed between the fan discharge and an elbow.

### Non-ducted Bower Inlets

The open inlet of a centrifugal fan too close to a wall or cabinet enclosure will reduce fan performance. Air is restricted and does not have easy access to the inlet. A minimum of one fan wheel diameter is recommended between the fan inlet and the wall. If two fans are installed within the same plenum or cabinet enclosure, and their inlets face each other, their inlets should be located a minimum of two wheel diameters apart.

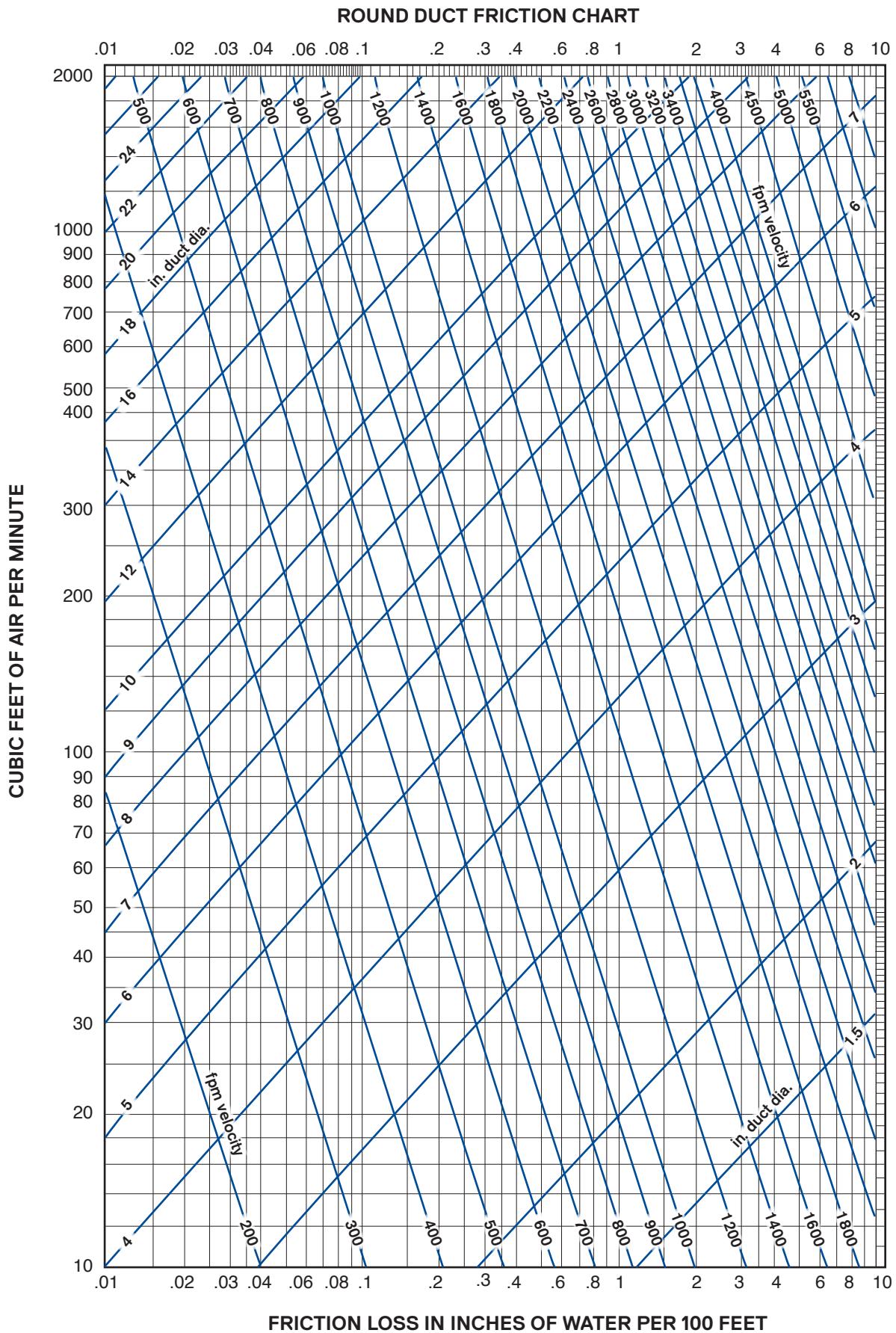
### Inlet Duct Turns

A duct turn (elbow) too close to the fan inlet reduces the fan's air performance. Air enters the fan inlet unevenly resulting in turbulence and limits the wheel's air handling efficiency. A minimum of one wheel diameter is recommended between the fan inlet and the end of the elbow if turning vanes have been installed. If there are no turning vanes in the elbow, a minimum of three wheel diameters should separate the fan inlet and the elbow.

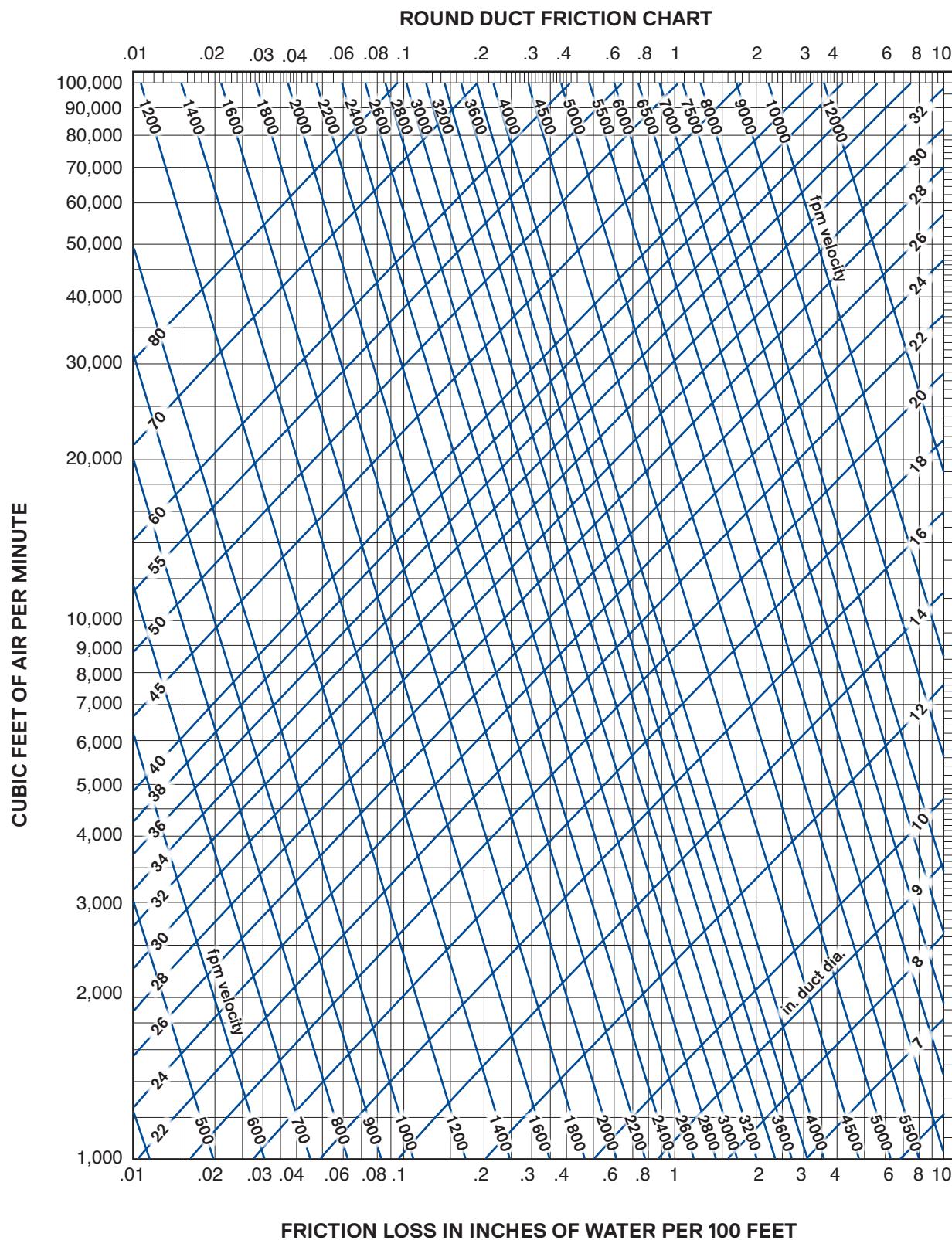
### Duct Inlet Spin

A major cause of reduced fan performance is an inlet duct connection that produces a spin or prerotation of the air entering the fan inlet. Inlet spin in the same direction of the fan wheel will reduce air volume and pressure ratings. Inlet spin in the opposite direction of the fan rotation will substantially increase the motor horsepower requirements. An ideal inlet condition is one which allows the air to enter the fan axially and evenly without spin in either direction.

## ESTIMATED STATIC PRESSURE – 10 TO 2000 CFM



## ESTIMATED STATIC PRESSURE – 1000 TO 100,000 CFM



## NOISE FACTORS

This section includes a general list of good practices to follow when selecting and installing fans to minimize the sound produced from their operation.

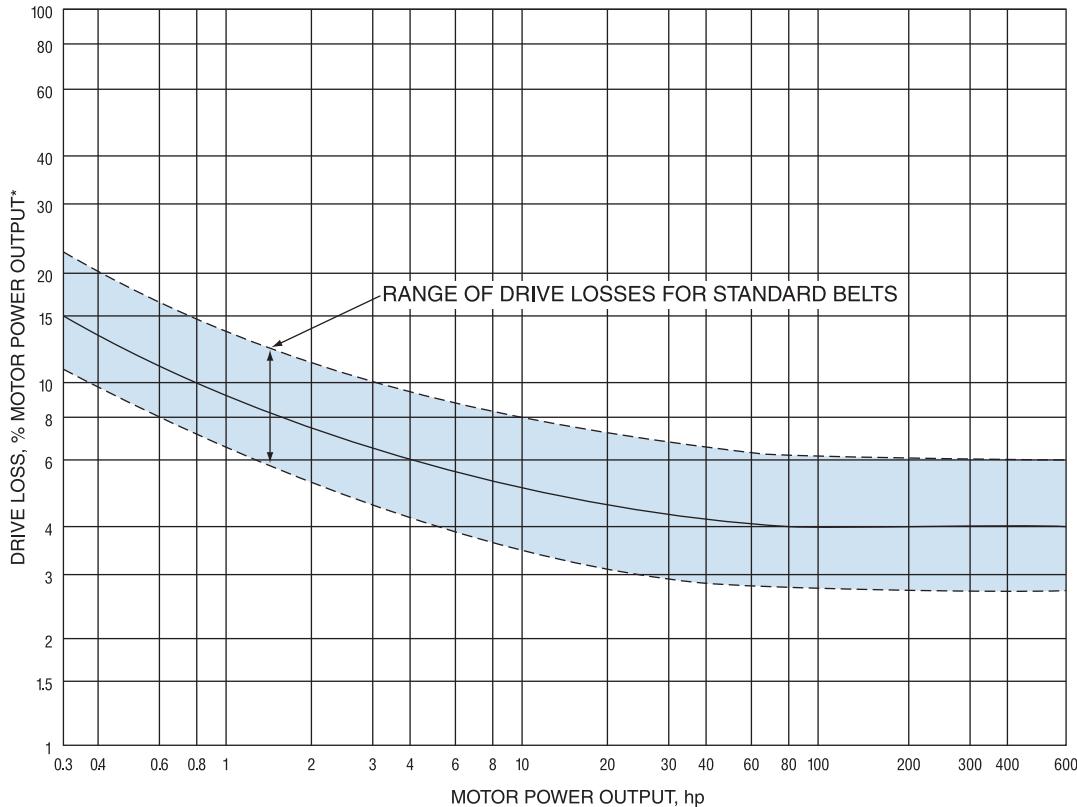
Check list for quiet operation:

- 1 Design the fan system for minimum resistance to air flow. Regardless of the type of fan used, sound generation increases with increases in static pressure.
- a Use larger heating or cooling coils, larger filter areas and larger size ducts.
- b Avoid abrupt changes in air velocity by using long transition pieces when changing to another size duct.
- c Avoid abrupt changes in direction of air flow by minimizing the number of turns in the duct run. If turns are required, use an elbow with a large turn radius and turning vanes. Minimum elbow radius should be equal to twice the duct diameter.
- d Make all duct runs as short and direct as possible.
- e Avoid elbows less than 4 wheel diameters away from fan discharge or less than 2 wheel diameters away from fan inlet.

- 2 Select a fan type suitable for the application.

- 3 When two sizes of the same fan type deliver the same air volume, select the larger size running at a slower speed.
- 4 Use vibration isolators and pads for fans and ductwork suitable for the application.
- 5 Avoid transmitting noise through a duct system. For general ventilation, inlet or outlet duct runs should not be directly connected to the fan. Isolate the connection with a rubber gasket. Whenever possible, leave a 1" gap between the fan and duct. Cover the gap with canvas or other suitable material to prevent air leaks.
- 6 Avoid mechanical noise.
  - a Tighten or strengthen vibrating panels.
  - b Keep bearings lubricated.
  - c Tighten belt(s) to proper tension. Do not overtighten.
  - d Align pulleys and shafts. Motor and fan shaft must be parallel.
  - e Tighten the se-screws in the wheel or impeller to their proper torque setting.
  - f Keep fan blades and wheels clean.
- 7 Locate fans away from people and the work area. Consider roof mounting.

## APPROXIMATE BELT DRIVE LOSSES



HIGHER BELT SPEEDS TEND TO HAVE HIGHER LOSSES THAN LOWER BELT SPEEDS AT THE SAME HORSEPOWER.

\* Drive losses are based on the conventional V-belt.













